

## Temperature calculations for heat transfer in extended surfaces (fins)

### Inputs:

Length of the cross-section:	$L_f := 100.0\text{mm}$
Width & height of cross-section:	$B_f := 2.0\text{mm}$ $H_f := 5.0\text{mm}$
Perimeter:	$\text{per} := 2 \cdot (H_f + B_f) = 14 \cdot \text{mm}$
Cross-section area:	$A_c := H_f \cdot B_f = 10 \cdot \text{mm}^2$
Heat transfer coefficient:	$h_c := 20.0 \frac{\text{W}}{\text{m}^2 \cdot \text{K}}$
Thermal conductivity of fin material:	$k_f := 200 \frac{\text{W}}{\text{m} \cdot \text{K}}$
Reference Temperature for HTC:	$T_{\text{REF}} := 40.0^\circ\text{C}$
Boundary condition base of the fin:	$T_B := 200^\circ\text{C}$
Type of boundary condition at tip:	Specified Temperature or insulated Other options can be: convective or infinite length
Boundary condition at tip of the fin:	$T_L := 100^\circ\text{C}$
Axial coordinate:	$x_f := 0, 2\text{mm}.. L_f$

### Derived parameters:

Fin constant:	$m_f := \sqrt{\frac{h_c \cdot \text{per}}{k_f \cdot A_c}} = 11.8 \cdot \frac{1}{\text{m}}$
	$M := \sqrt{h_c \cdot \text{per} \cdot k_f \cdot A_c} = 0.024 \cdot \frac{\text{W}}{\text{K}}$
Non-dimensional Temperatures:	$\theta_B := T_B - T_{\text{REF}} = 160 \text{ K}$
	$\theta_L := T_L - T_{\text{REF}} = 60 \text{ K}$

### Functions for temperature and heat fluxes:

BC1: Specified convection at tip	$\theta_1(x) := \theta_B \cdot \frac{\cosh[m_f \cdot (L_f - x)] + \frac{h_c}{m_f \cdot k_f} \cdot \sinh[m_f \cdot (L_f - x)]}{\cosh(m_f \cdot L_f) + \frac{h_c}{m_f \cdot k_f} \cdot \sinh(m_f \cdot L_f)}$
$T_1(x) := \theta_1(x) + T_{\text{REF}}$	

BC2: Specified temperature at tip

$$\theta_2(x) := \theta_B \cdot \frac{\left(\frac{\theta_L}{\theta_B} + 1\right) \cdot \sinh[m_f \cdot (L_f - x)]}{\sinh(m_f \cdot L_f)} \quad T_2(x) := \theta_2(x) + T_{REF}$$

BC3: Insulated tip

$$\theta_3(x) := \theta_B \cdot \frac{\cosh[m_f \cdot (L_f - x)]}{\cosh(m_f \cdot L_f)} \quad T_3(x) := \theta_3(x) + T_{REF}$$

BC4: Infinitely long fin (for  $L_f \gg B_f$ )

$$\theta_4(x) := \theta_B \cdot e^{-m_f \cdot x} \quad T_4(x) := \theta_4(x) + T_{REF}$$

*Heat flux through base of the fin:*

BC1: Specified convection

$$q''_{B1}(h_c) := \sqrt{h_c \cdot \text{per} \cdot k_f \cdot A_c} \cdot \theta_B \cdot \frac{\sinh\left(\sqrt{\frac{h_c \cdot \text{per}}{k_f \cdot A_c}} \cdot L_f\right) + \sqrt{\frac{h_c \cdot A_c}{k_f \cdot \text{per}}} \cdot \cosh\left(\sqrt{\frac{h_c \cdot \text{per}}{k_f \cdot A_c}} \cdot L_f\right)}{\cosh\left(\sqrt{\frac{h_c \cdot \text{per}}{k_f \cdot A_c}} \cdot L_f\right) + \sqrt{\frac{h_c \cdot A_c}{k_f \cdot \text{per}}} \cdot \sinh\left(\sqrt{\frac{h_c \cdot \text{per}}{k_f \cdot A_c}} \cdot L_f\right)}$$

BC2: Specified temperature

$$q''_{B2}(h_c) := \sqrt{h_c \cdot \text{per} \cdot k_f \cdot A_c} \cdot \theta_B \cdot \frac{\cosh\left(\sqrt{\frac{h_c \cdot \text{per}}{k_f \cdot A_c}} \cdot L_f\right) - \frac{\theta_L}{\theta_B}}{\sinh\left(\sqrt{\frac{h_c \cdot \text{per}}{k_f \cdot A_c}} \cdot L_f\right)}$$

BC3: Insulated tip

$$q''_{B3}(h_c) := \sqrt{h_c \cdot \text{per} \cdot k_f \cdot A_c} \cdot \theta_B \cdot \tanh\left(\sqrt{\frac{h_c \cdot \text{per}}{k_f \cdot A_c}} \cdot L_f\right)$$

BC4: Infinitely long fin (for  $L_f \gg B_f$ )

$$q''_{B4}(h_c) := \sqrt{h_c \cdot \text{per} \cdot k_f \cdot A_c} \cdot \theta_B$$

Heat flux through tip of the fin:

BC1: Specified convection

$$q''_{t1} := h_c \cdot A_c \cdot \theta_L$$

BC2: Specified temperature

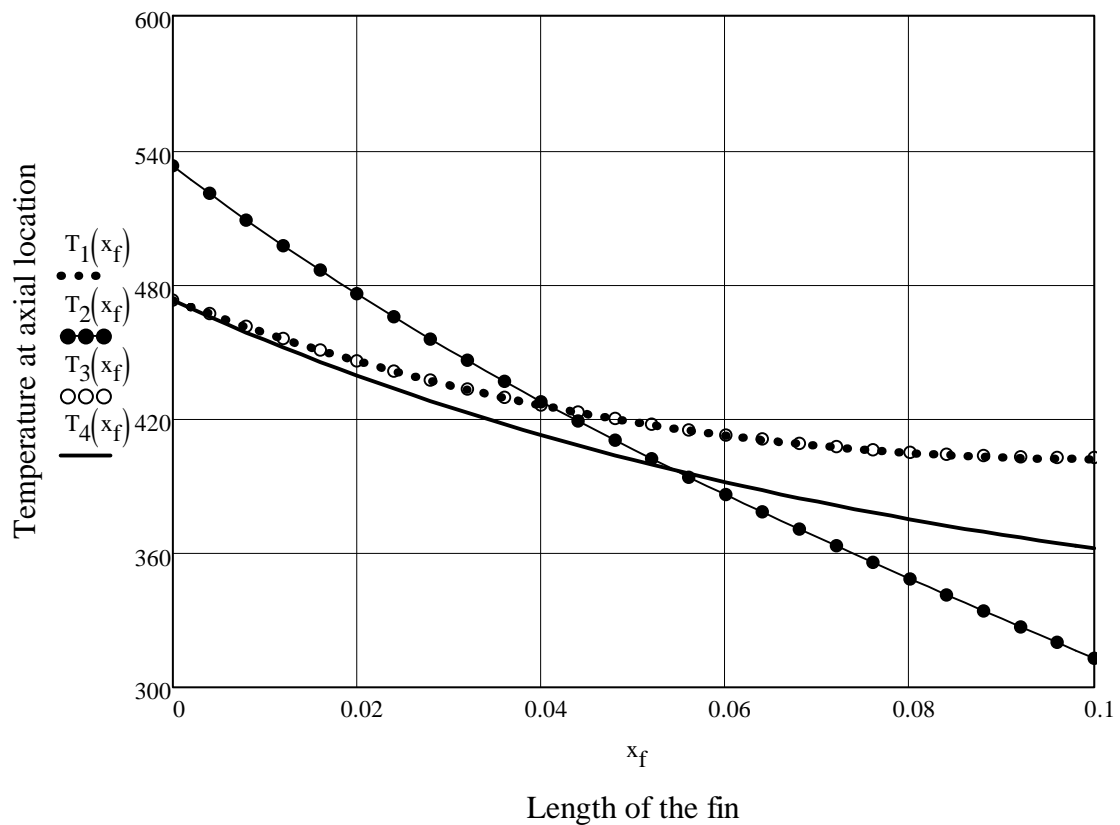
$$q''_{t2} := \frac{M \cdot (\theta_B + \theta_L)}{\sinh(m_f \cdot L_f)}$$

BC3: Insulated tip

$$q''_{t3} := 0.0$$

BC4: Infinitely long fin (for  $L_f \gg B_f$ )

$$q''_{t4} := 0.0$$



$$\frac{h_c}{m_f \cdot k_f} = 0.008 \ll 1.0$$

And hence, the temperature profiles for tip conditions "specified convection" and 'insulated' are same as one may have expected (shown by overlapping lines in the plot above).

$$h_c := 0,1 \frac{W}{m^2 \cdot K} \dots 50 \frac{W}{m^2 \cdot K}$$

